

REINHOLD ENVIRONMENTAL Ltd.



**2015 APC Round Table
& Expo Presentation**

July 13 & 14, 2015, in Atlanta, GA / Hosted by Southern Company

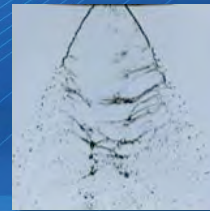
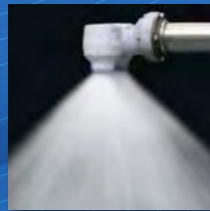
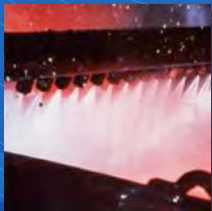
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**ENGINEERING
YOUR SPRAY SOLUTION**



Successful Operation of Flue Gas Humidification/Cooling Using Spray Nozzles Upstream of DSI

Robert Van Durme, P.E.



What is DSI

The Challenges of Upstream Cooling

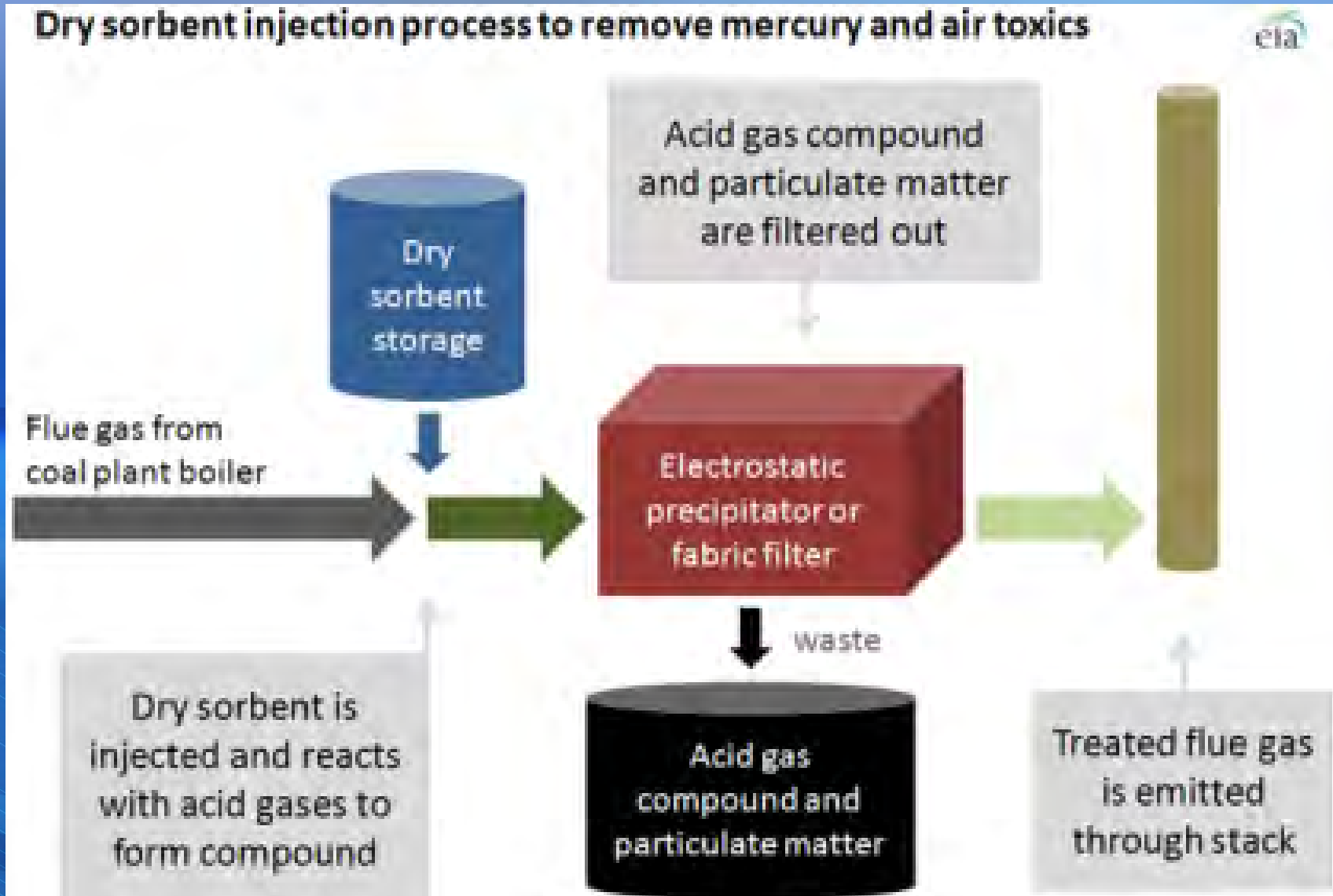
Fluid Application Engineering

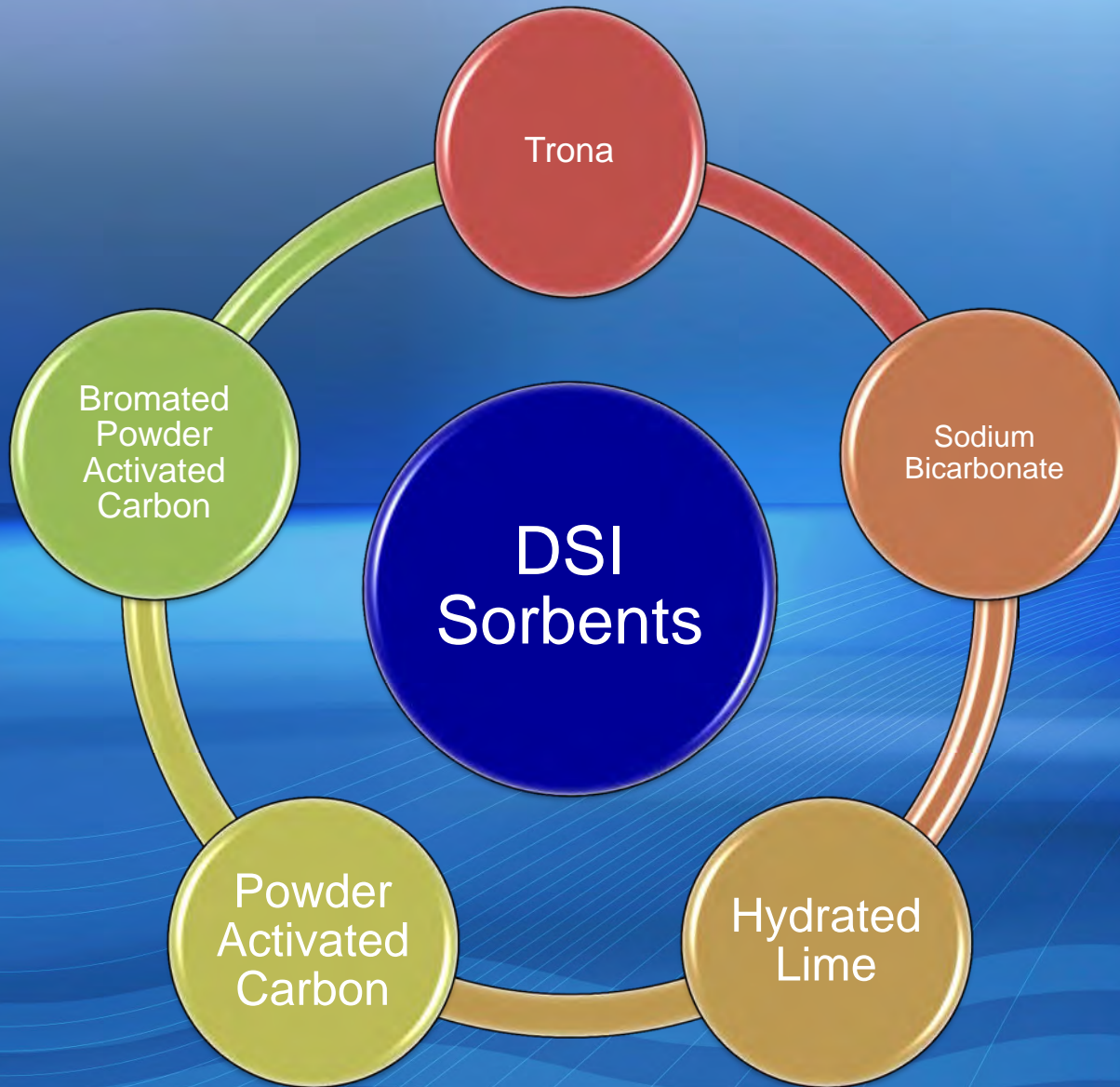
Comparison of Nozzle Technologies

Case Study

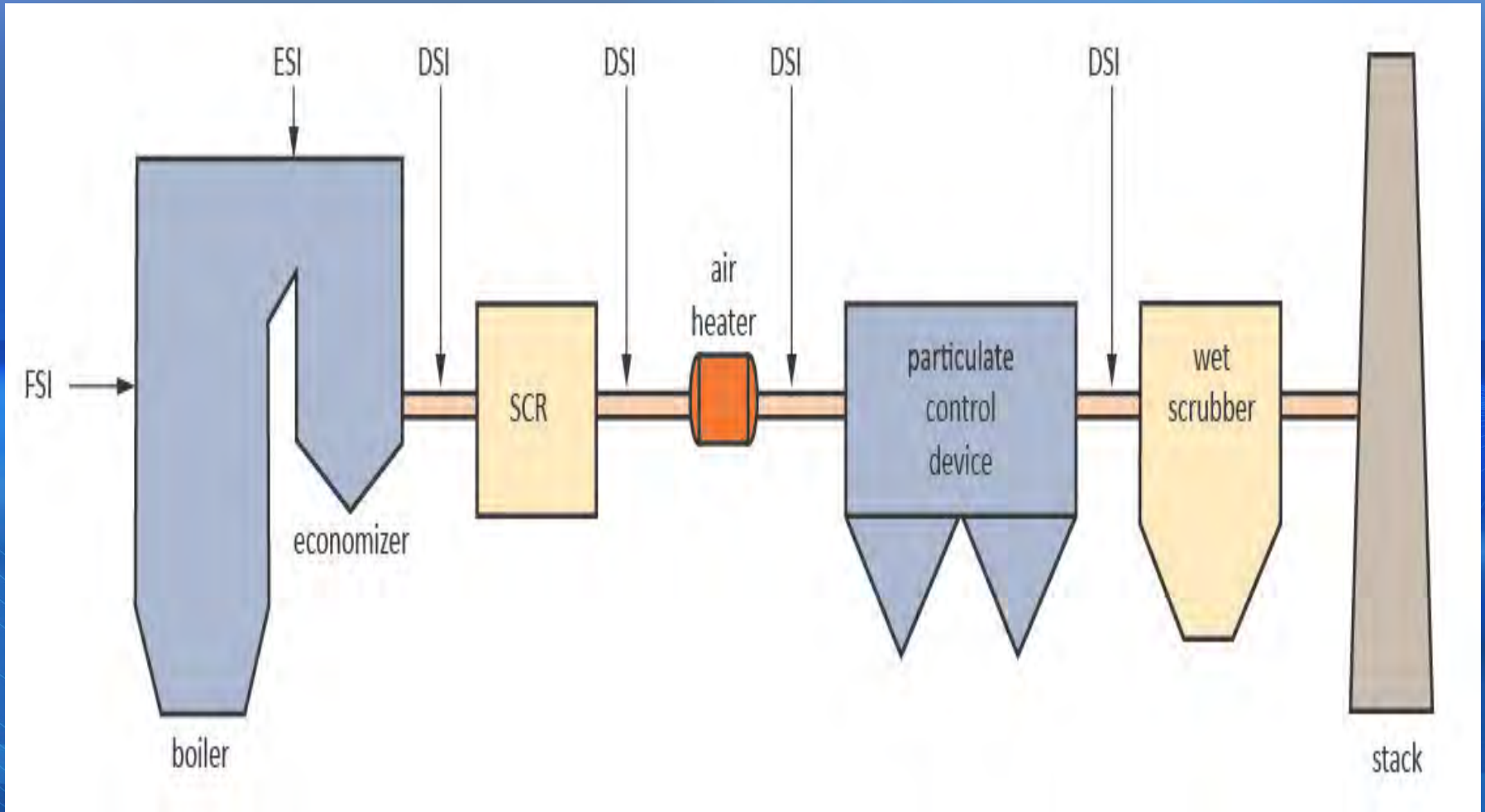
Question & Answer

Dry sorbent injection process to remove mercury and air toxics





What is DSI....



	Upper Furnace	Superheater/ Reheater	ECON	Air Heater
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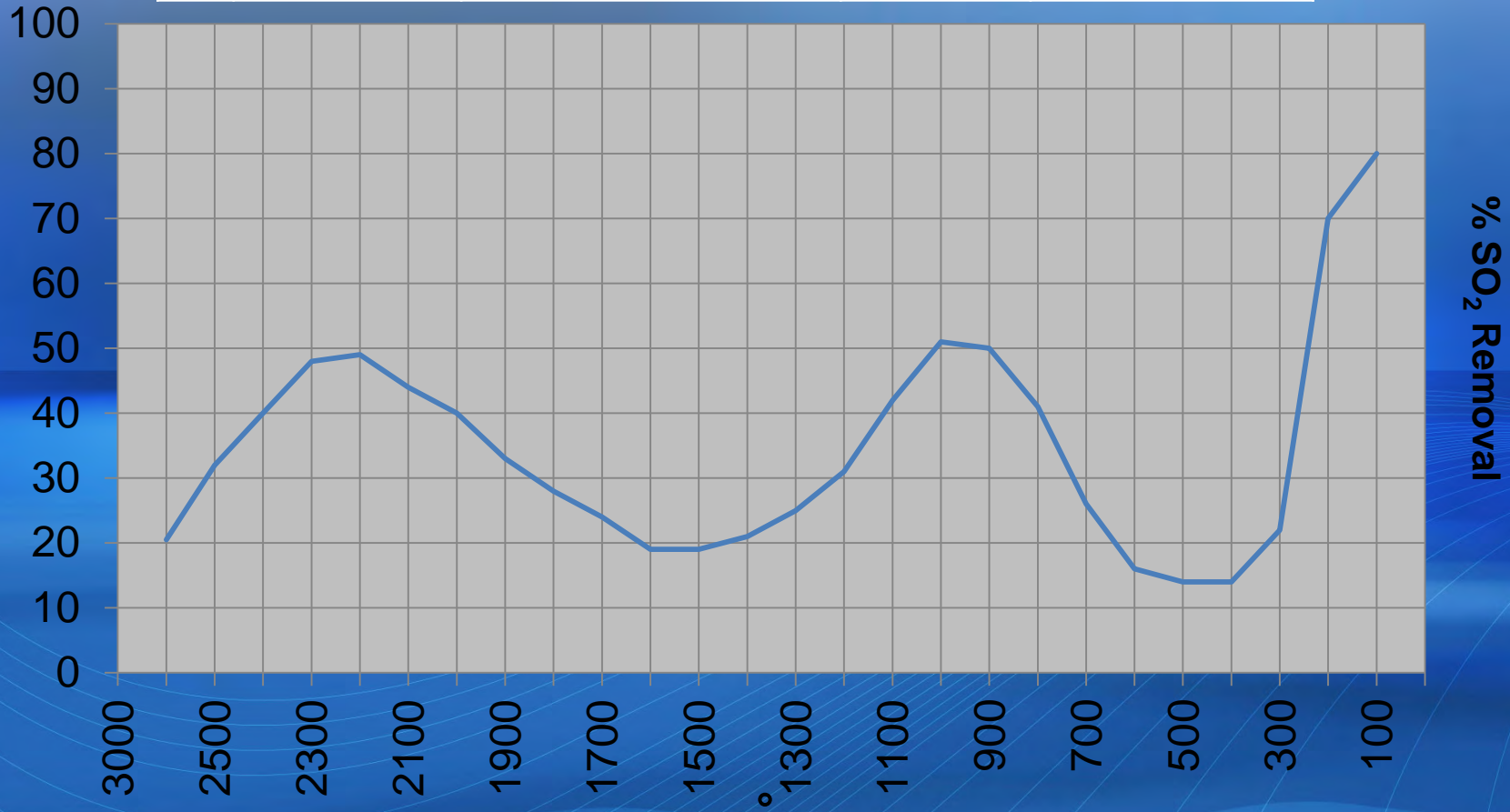


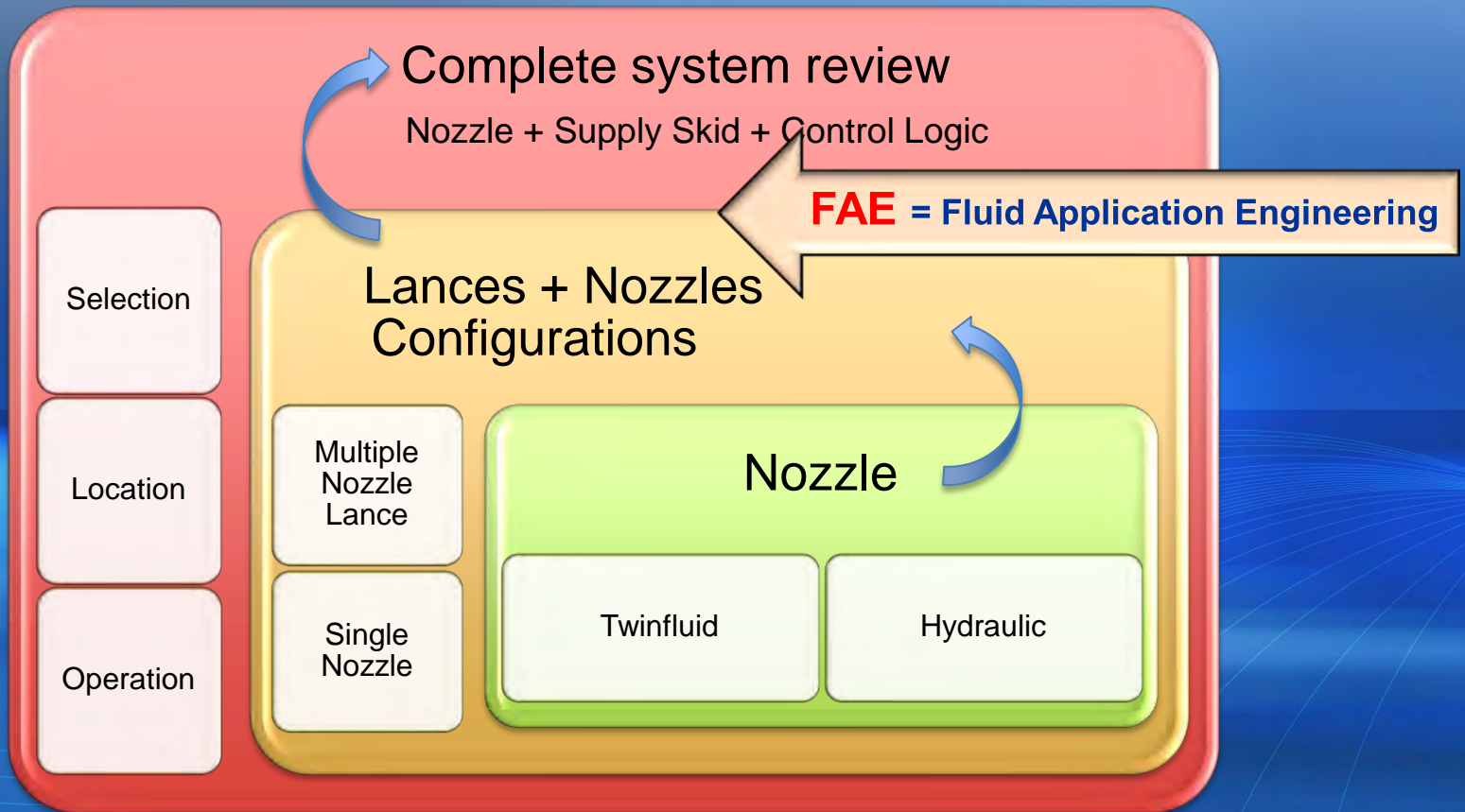
Figure 1 - SO₂ Removal As A Function of Flue Gas Temperature at Ca/S of 2.0 - Dry Sorbent FGD – Calcium Based Reagents (1)





Anyone
can do it!

Due diligence needs to be performed...



From components to systems – from small to big
The complete system must be matched to perform

Selection

Droplet Size

Twinfluid/Hydraulic

Operating Pressure

Spray Angle

Turndown

Material

Turndown Ratio

Free passage

Location

Evaporation Distance

Coverage

Orientation

Gas Distribution

Temperature

Duct Geometry

Accessibility

Operation

Steady-state

Process Fluctuations

Control Logic

Redundancy

Fail-safe

Maintenance

Nozzle Wear

Durability

Twinfluid

**Twinfluid with Ring
Gap Technology**

Hydraulic

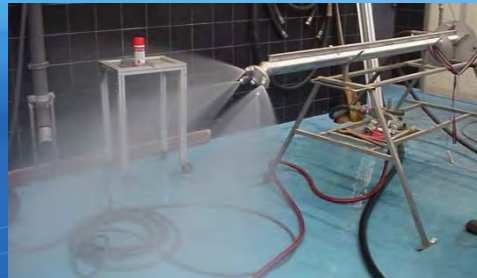
Spillback



Spray Nozzle Types

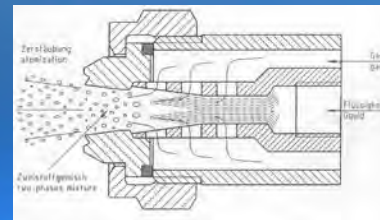
Air Atomizing – shearing liquid into droplets with a high velocity air stream using compressed air

Hydraulic Atomizing – shearing a high velocity sheet of liquid into droplets by the relative velocity of the adjacent, relatively stationary, air.



Atomizing Method / Turn-down / Droplet Size

Air Atomizing / $< 40:1$ / as small as 20 micron SMD , 80 -100 psi

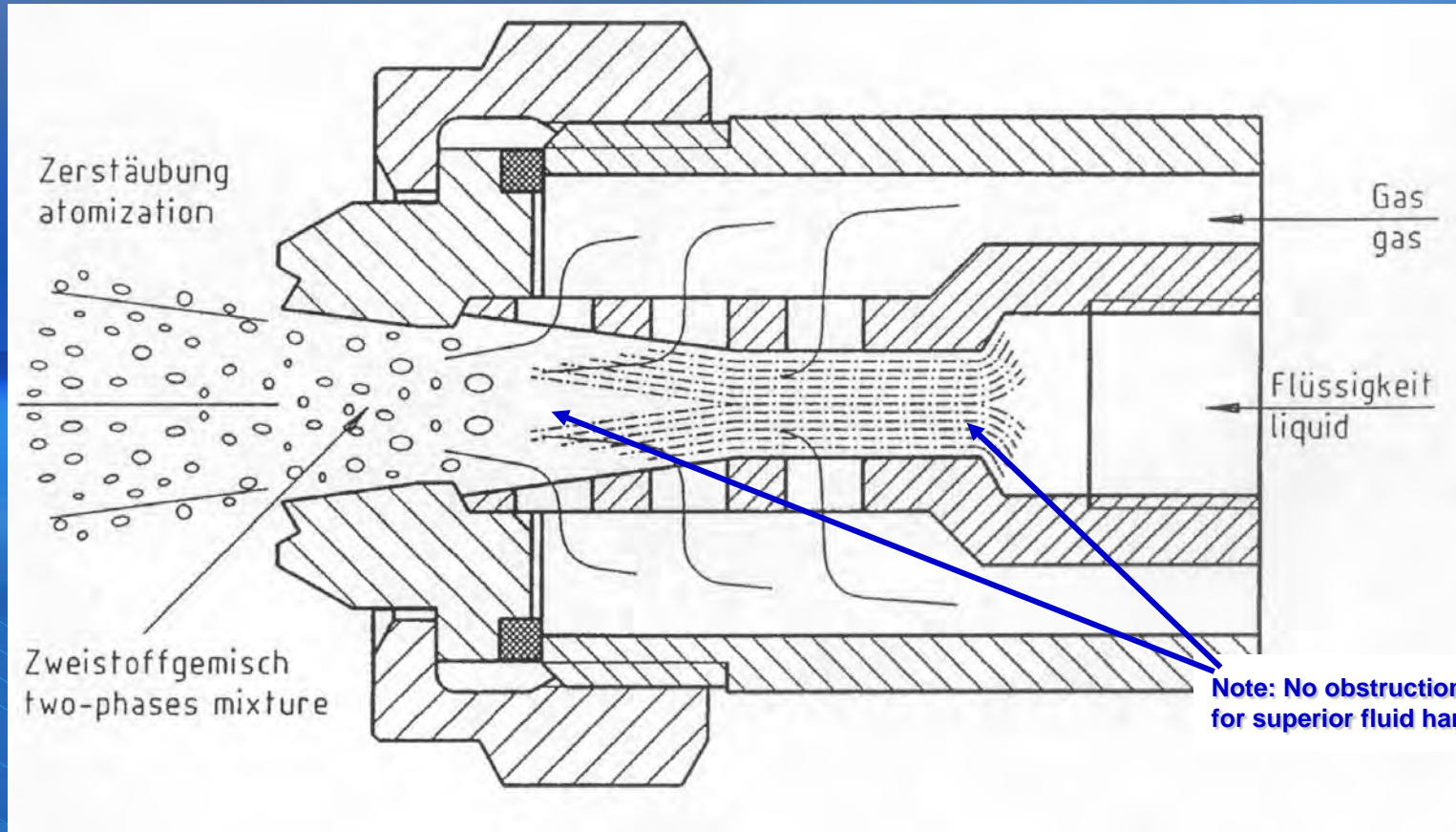


Simple Hydraulic / $< 3:1$ / as small as 30 micron SMD , 2500 psi, < 1 gpm

**Spillback (Return Flow) Hydraulic / $10:1$ / as small as 100 micron SMD
rated capacity dependent at full flow**



Lechler Nozzle: Twin Fluid - Laval-Type (internal mixing)

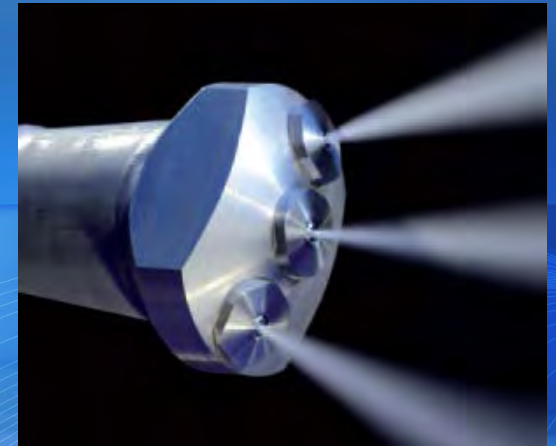


Comparison of Nozzle Technologies

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Lances and systems for humidification/cooling can be single point or multiple nozzle configuration to ensure proper spray coverage



A barrier air pipe can cover entire lance and provide low pressure (~ .5 psig) air supply to keep nozzle orifice clean from buildup



Parameters which Influence Droplet Size – Air atomizing

Higher Air/Liquid mass ratio provides smaller droplets

Higher air pressure can provide a narrow droplet spectrum

For a given flow rate and droplet size, choose the smallest capacity nozzle operated at the highest air pressure to use the lowest amount of air

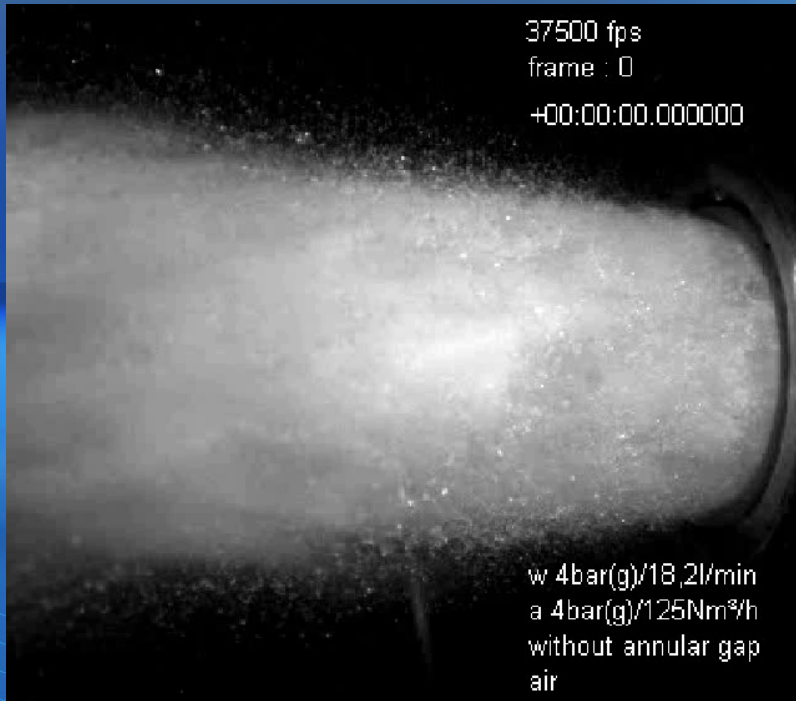


Standard Twinfluid

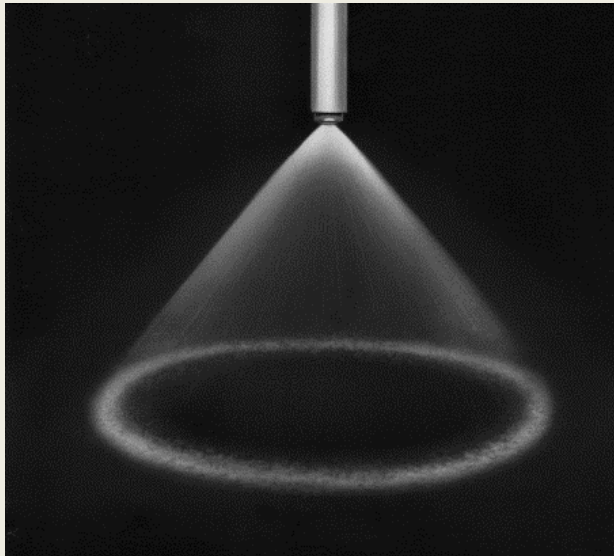


Standard Twinfluid with Ring Gap

Ring Gap Technology

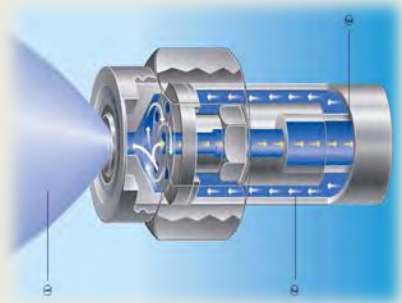


Hydraulic Nozzle



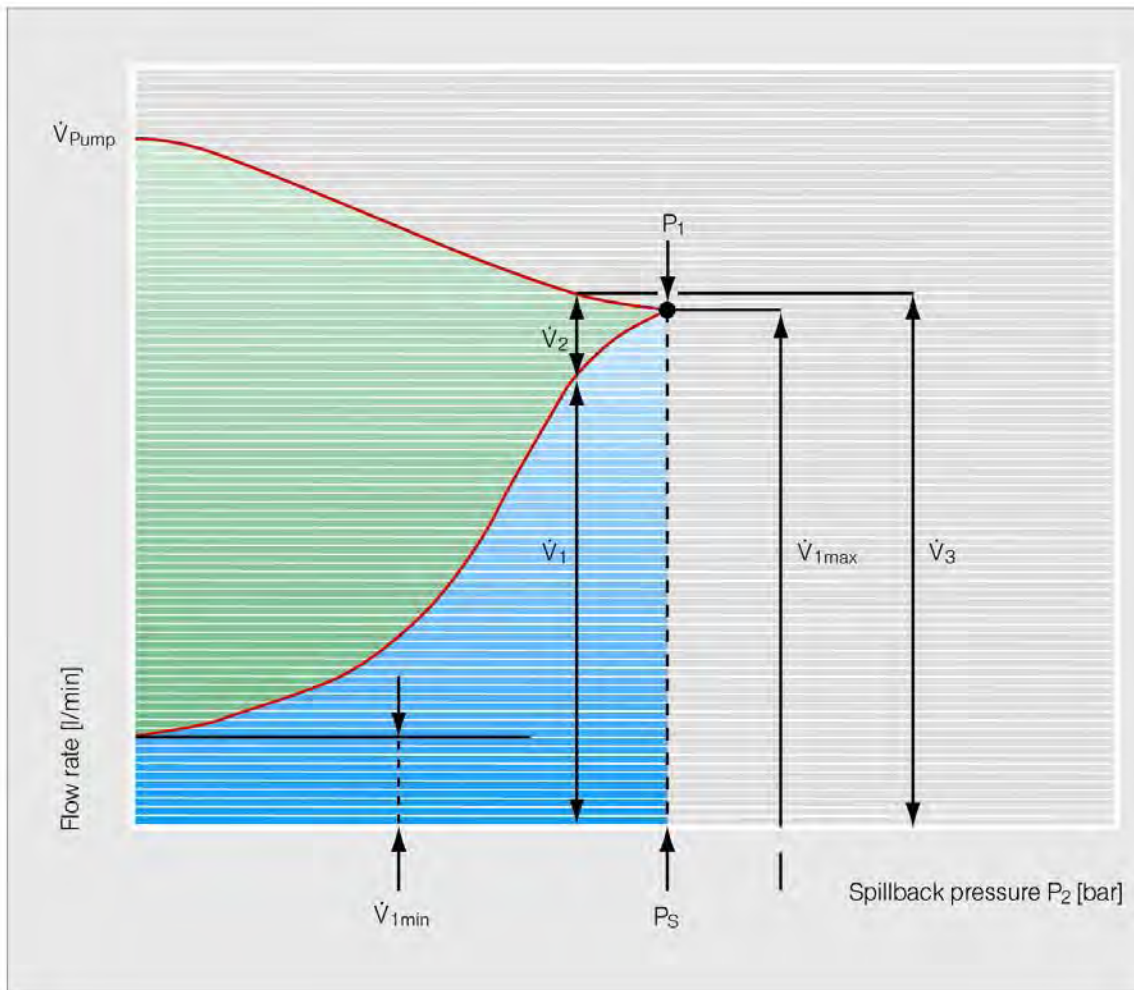
- Finely atomized hollow cone spray is produced by pump pressure orifice.
- The droplet size is proportional to the supply pressure
- D_{max} can be several times greater than twinfluid or Spillback technology
- Regulation of the spray volume is achieved by adjusting supply pressure.

Spillback Nozzle



- Finely atomized hollow cone spray is produced by balancing the flow through the nozzle orifice and the return line.
- The high pressure liquid feed flow produces a uniform spray angle and $D_{max} < 300 \mu m$ over the entire range of flow.
- Regulation of the spray volume is achieved by adjusting a control valve on the return line.

Spillback Nozzle



- \dot{V}_1 = Sprayed volume
 - \dot{V}_{1max} = Max. sprayed volume (return line closed)
 - \dot{V}_{1min} = Min. sprayed volume (return line completely open)
 - \dot{V}_2 = Spillback flow rate
 - \dot{V}_3 = Pump delivery
 - \dot{V}_{Pump} = Pump delivery per nozzle
 - P_1 = Constant feed pressure
 - P_2 = Spillback pressure
 - P_S = Spillback pressure at \dot{V}_{1max} (P_{max} for control valve)
- Turn down ratio = $\dot{V}_{1max} / \dot{V}_{1min}$.



Droplet Size Characterization



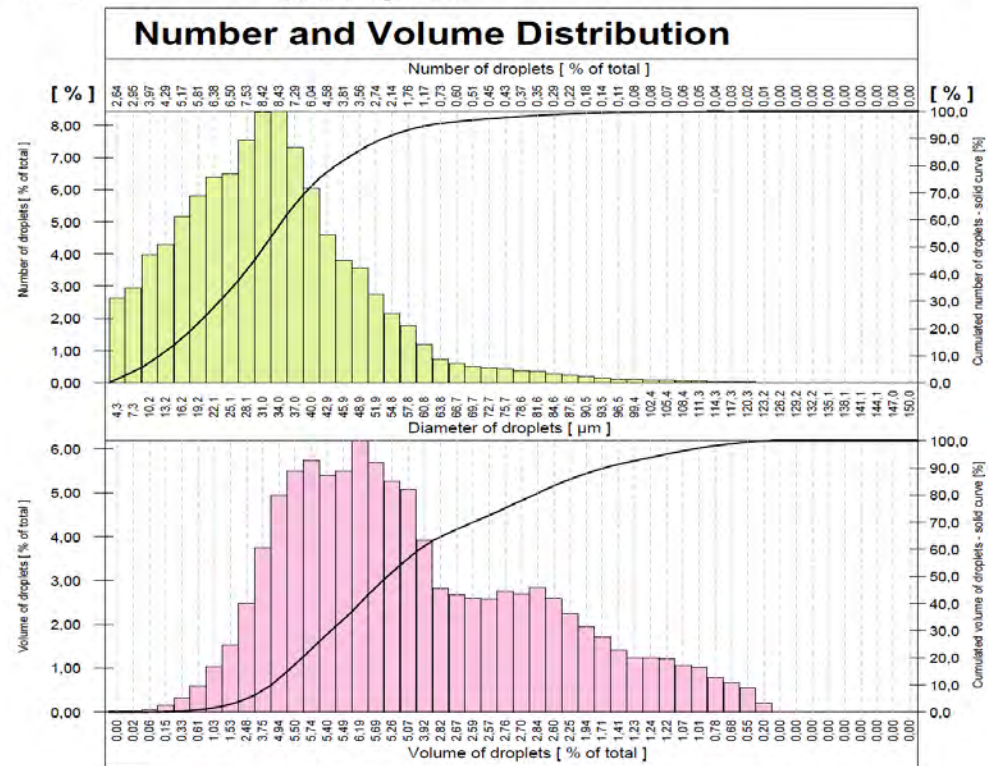
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Droplet Size Analysis

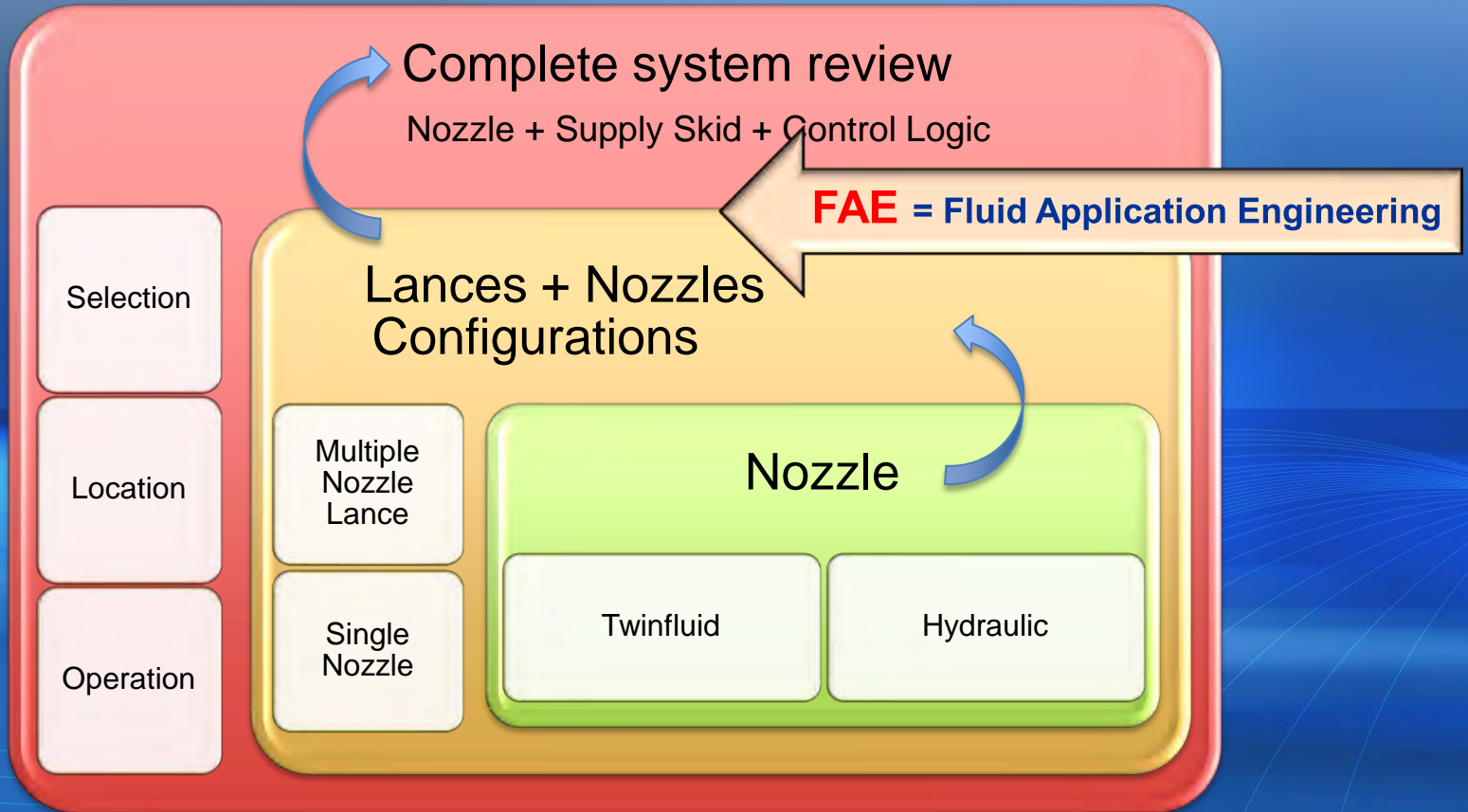
Product number 170.961.30
Date of measurement 7 JUL 1999
Liquid pressure 4,84 bar
Liquid flowrate 25,00 l/min
Gas pressure 5,00 bar
Gas flowrate 248,60 m³/h i.N.
Gas/Liquid ratio 9,94 [(m³/h)/(l/min)]
Meas.location (x/y/z) -/-/800 [mm]
Medium Wasser
Distribution type -----

Number of droplets = 14229
Arithmet. mean value = 32,54 µm
Standard deviation = 52,06 %
Area mean diameter = 36,68 µm
Volume mean diameter = 40,65 µm
D(Num)10% = 10,54 µm
D(Num)50% = 29,76 µm
D(Num)90% = 51,75 µm
D(VOL) 10% = 31,08 µm
D(VOL) 50% = 52,48 µm
D(VOL) 90% = 92,42 µm
Sauter mean diameter = 49,92 µm

Remark querschnittsgemittelt;



Due diligence needs to be performed...



From components to systems – from small to big
The complete system must be matched to perform

Successful operation of flue gas humidification/cooling using spray nozzles upstream of Dry Sorbent Injection (DSI)

Robert Van Durme, P.E. – Lechler Inc., Key Account Manager

Leon Lenertz, P.E. – Xcel Energy – Red Wing Station, Operations Manager

Ashwin Patni – Lechler Inc., Key Account Manager

Xcel Energy Red Wing Station Unit 1 & 2

Plant Data

Plant Issues and Opportunities for Improvement

Modeling

Results & Findings



Xcel Energy Red Wing Station Unit 1 & 2

Design Data

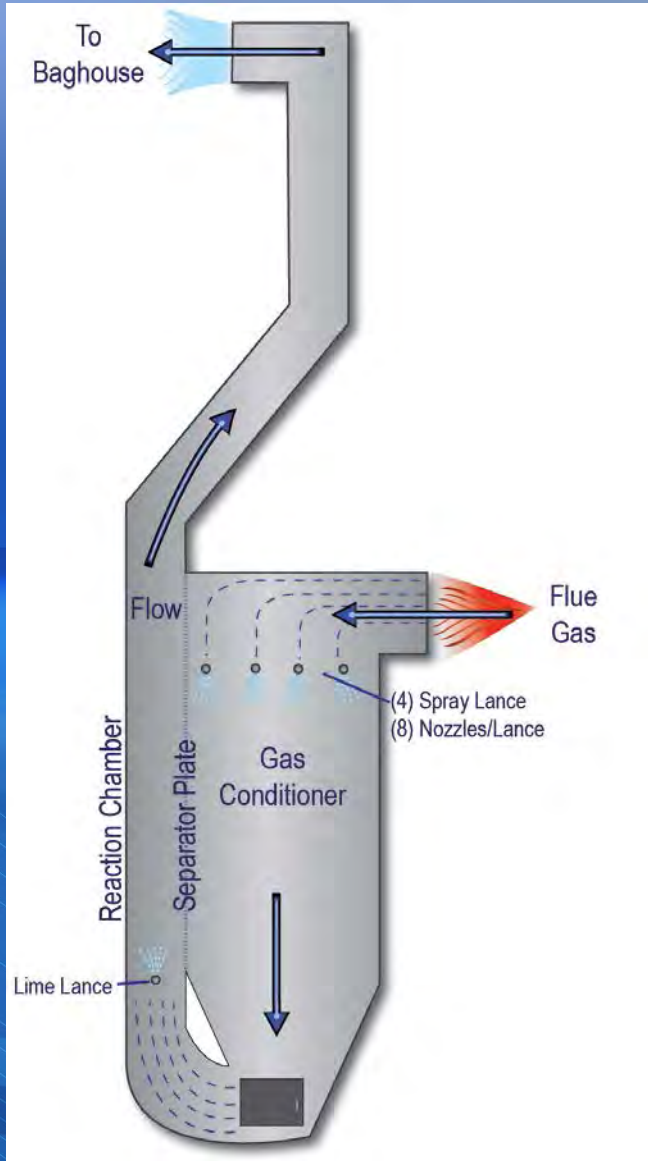
- Each Unit Size: 12MW
- Original built as coal-fired generation plant
- Currently burns RDF (Refuse-Derived Fuel)

In-Duct Scrubber

- Flue gas design flowrate: 110,000 ACFM
- Total water feed flowrate at design 24 gpm/unit
- Total compressed air: ~ 1,500 SCFM
- ~ 425° Preheater Outlet
- ~ 285° Baghouse Inlet
- Approximate lime usage: 4,500 tons/year



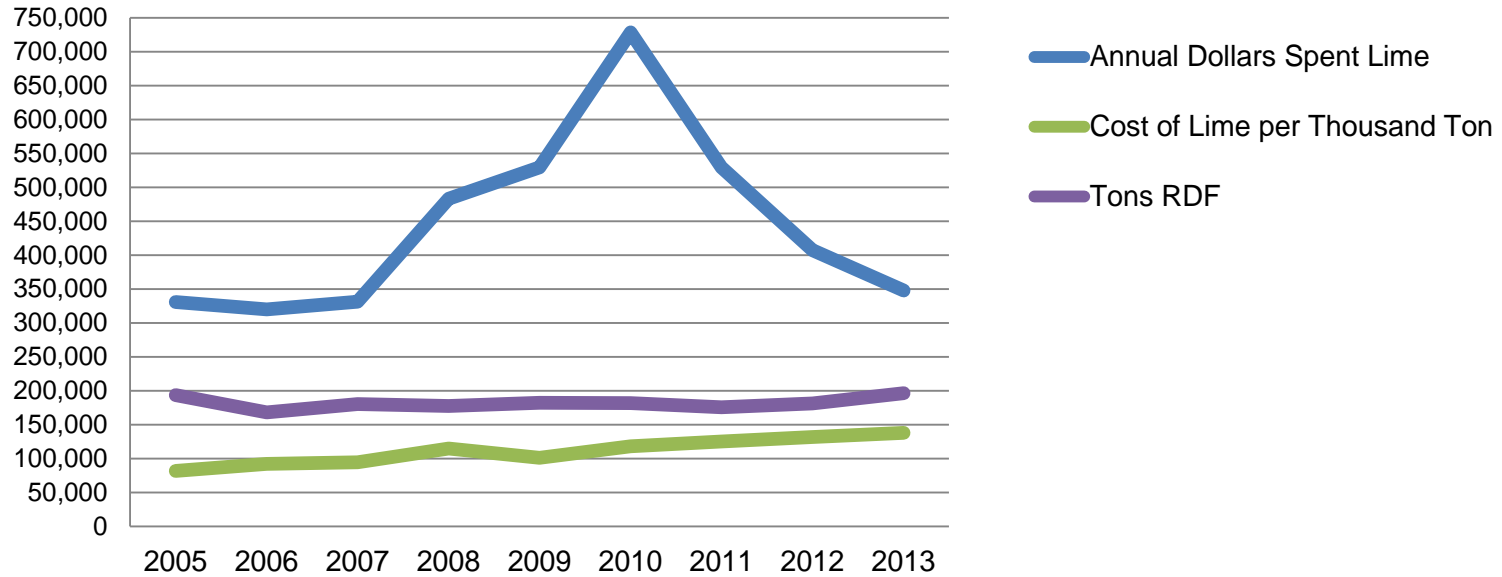
Red Wing Plant Data (cont'd)



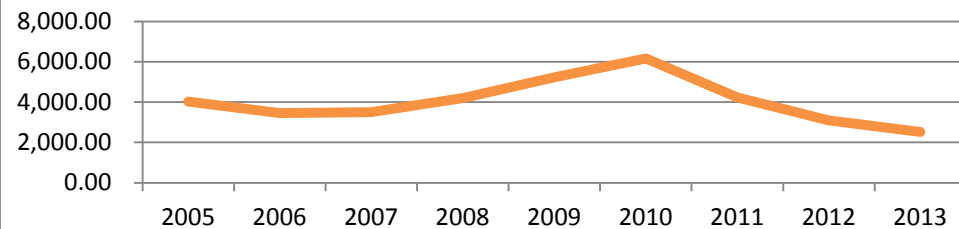
Red Wing Plant Data (Cont'd) Annual Lime Usage and Expense



Annual Lime Expense



Lime Usage (tons)



- High energy costs for compressed air usage: 1,500 SCFM (750 SCFM/unit)
- Maintenance costs for air compressor: \$ 25,000+ annually
- Increasing lime usage/costs: \$ 700,000 annually
- Nozzles: High maintenance and man-hours for servicing
- Reaching bag temperature limit



*Many
tough
problems
are
overcome
by
leniency*

~ Ali bin Abi Talib

High Compressed Air Usage

Nozzle design issue

High Maintenance Costs

Air compressor required

Frequent maintenance

Premature Nozzle Wear

316SS nozzle material construction, not suitable for process conditions

Acid gas condensation on metal surfaces

Duct Wetting

Incorrect nozzle/lance layout inside ductwork



Why duct humidification/cooling prior to DSI?

- Improve reactivity rates with reduced gas temperature
- Reduce fan power usage
- Lower operating costs via lower temperature bags
- Reduce sorbent usage/type
- Reduce ESP loading

What's the catch....hasn't this been tried before?

- Duct wetting
- Duct corrosion
- Buildup and pluggage
- Reliability issues



2010

- Droplet size modeling

2011

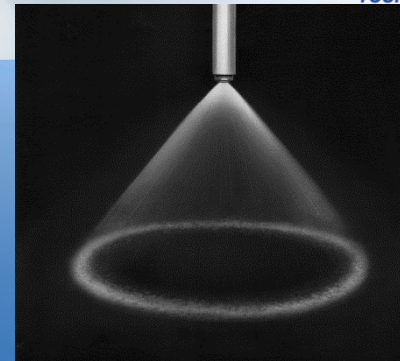
- Installed test nozzles
- Installed 2 complete set of nozzle twinfluid lances

2012-2013

- Converted to hydraulic-only lance design

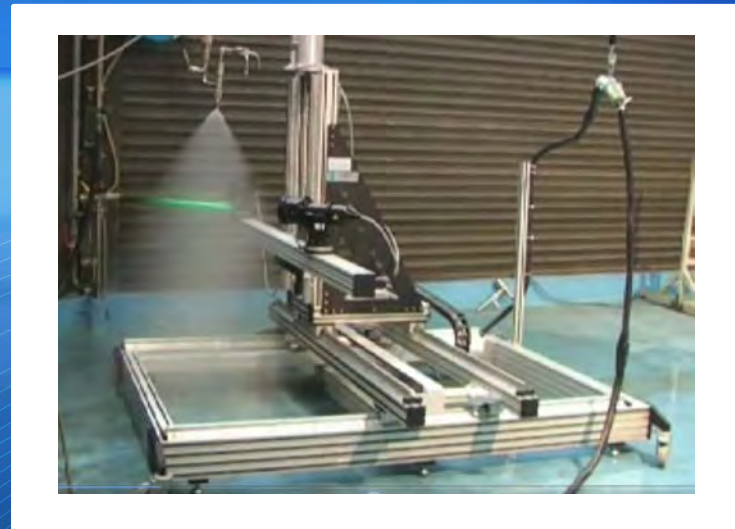
Original Lances

- Aggressive corrosion of base material



PDPA

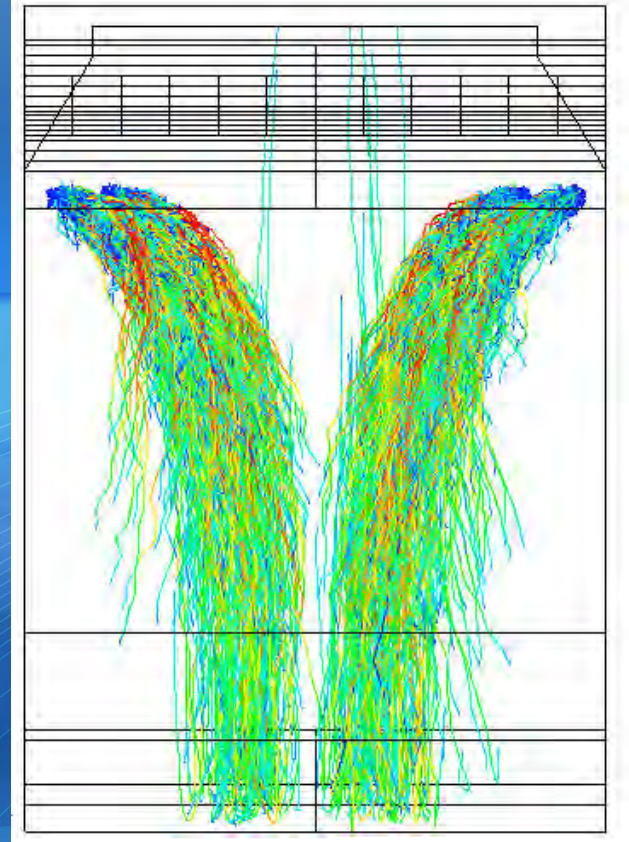
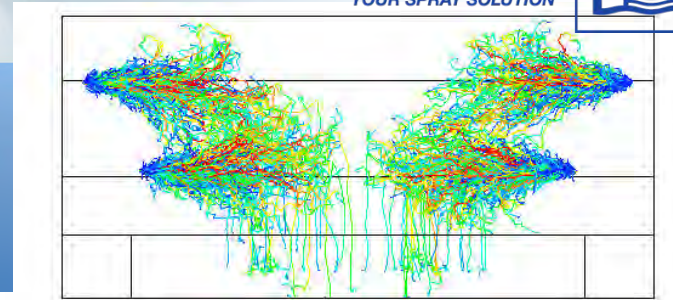
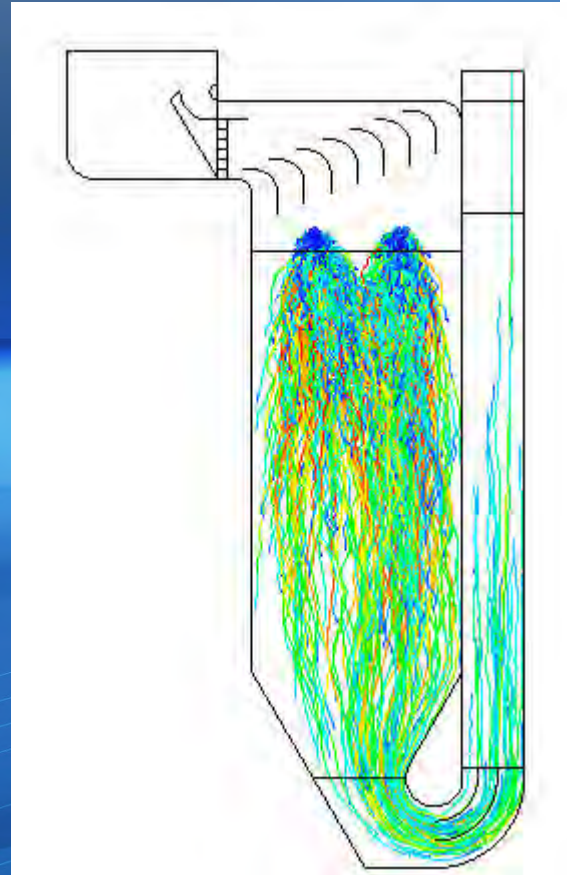
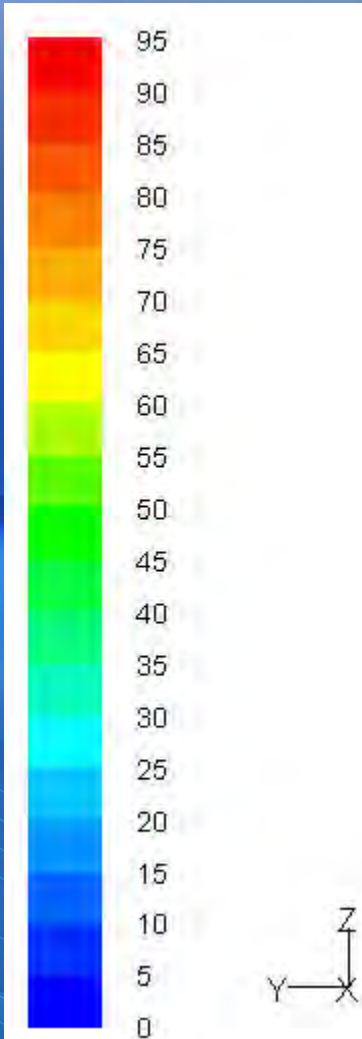
- Phase Doppler Particle Analyzer

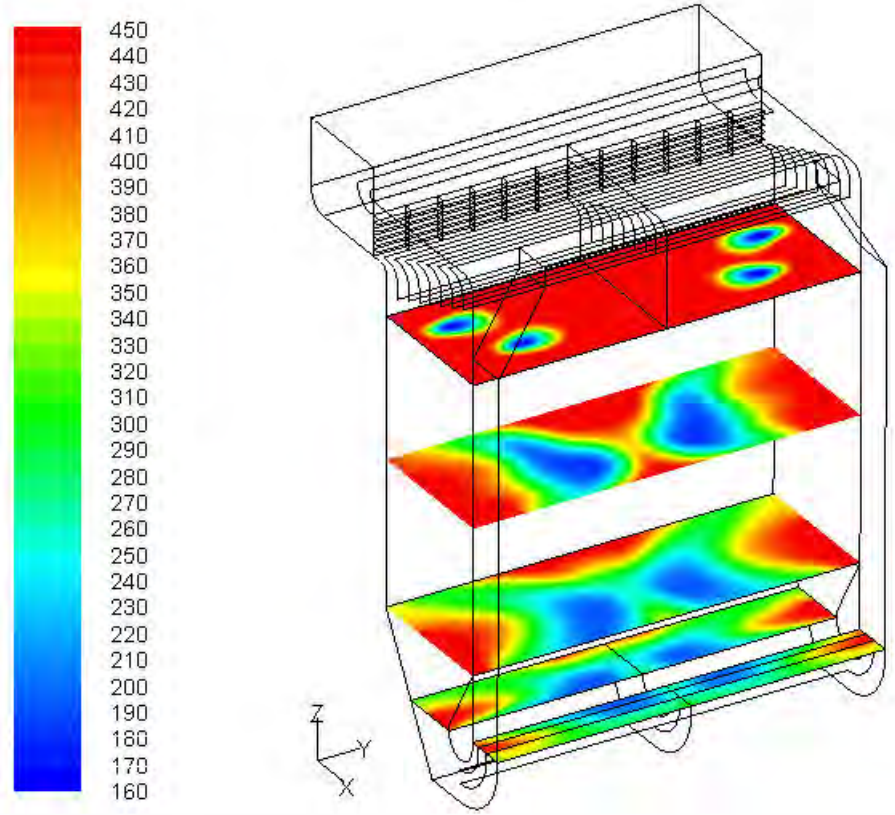


Case Study - Modeling

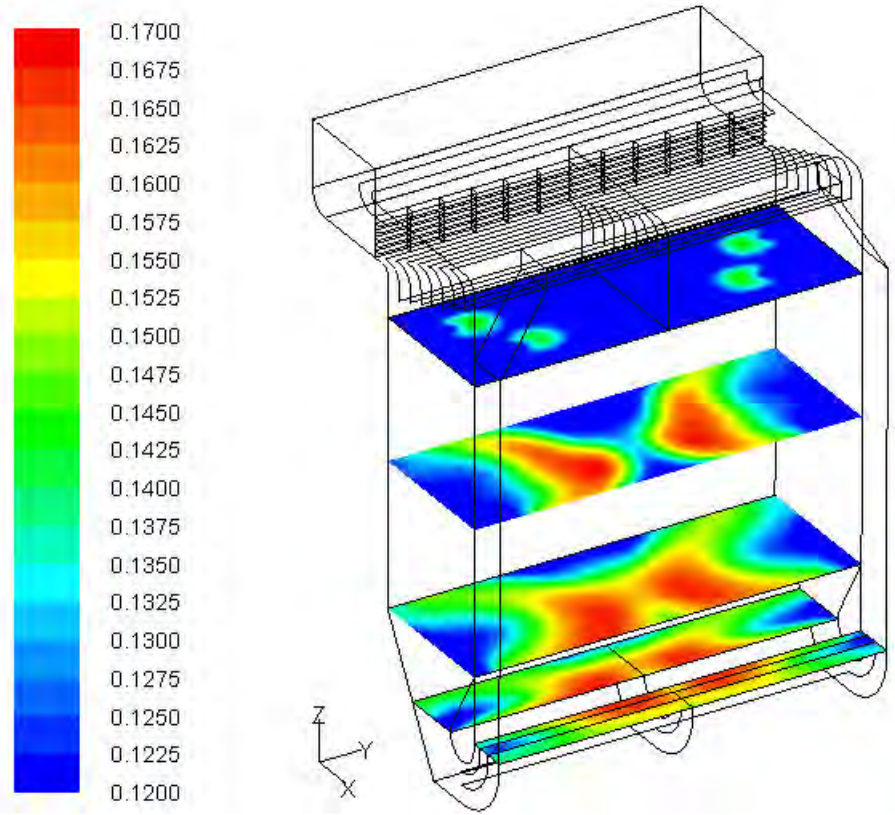
With 3,200 droplets tracked, only a few carry-over into the reaction chamber.

Droplet Diameter (microns)



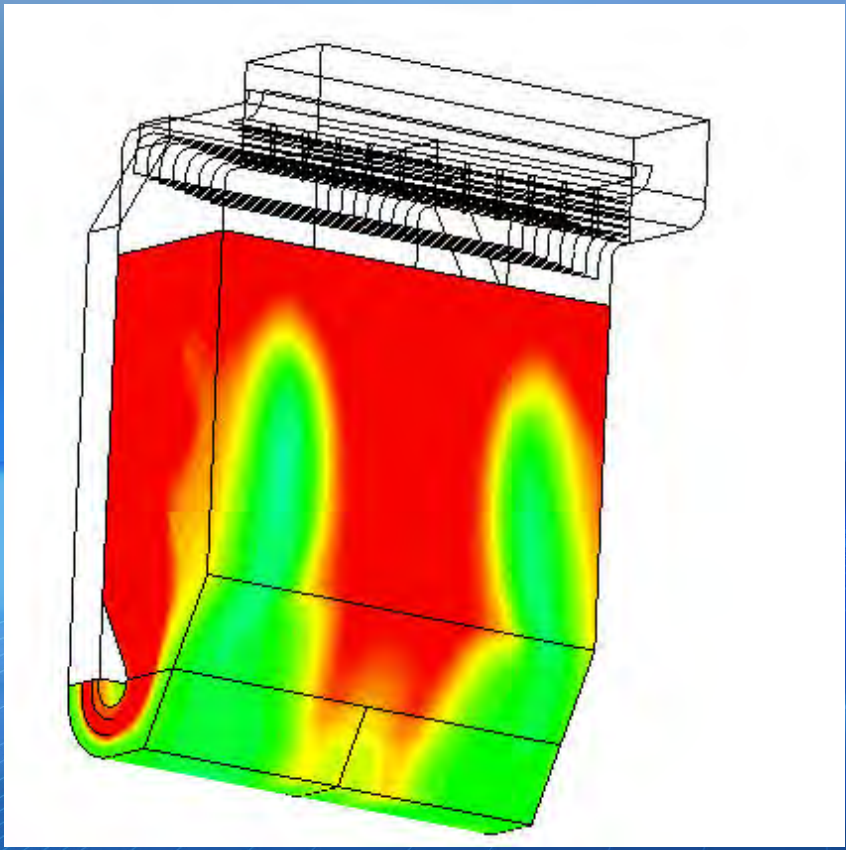
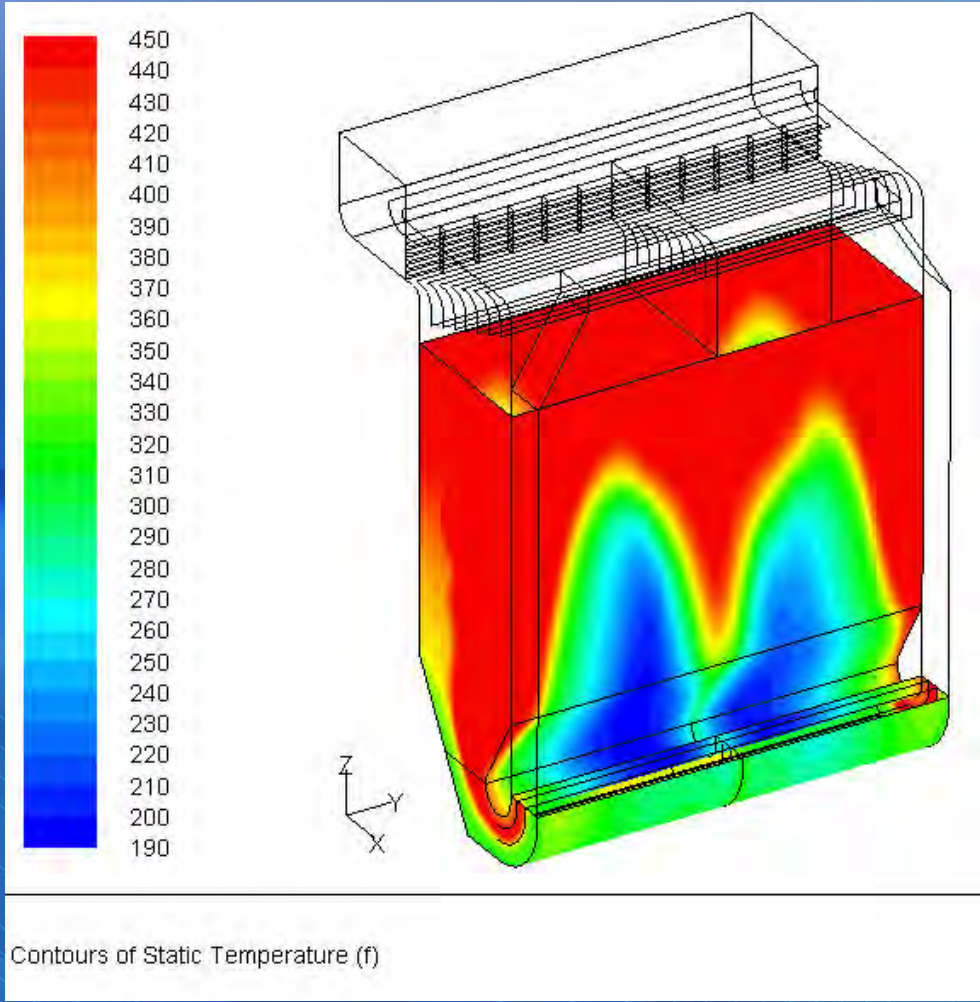


Contours of Static Temperature (f)

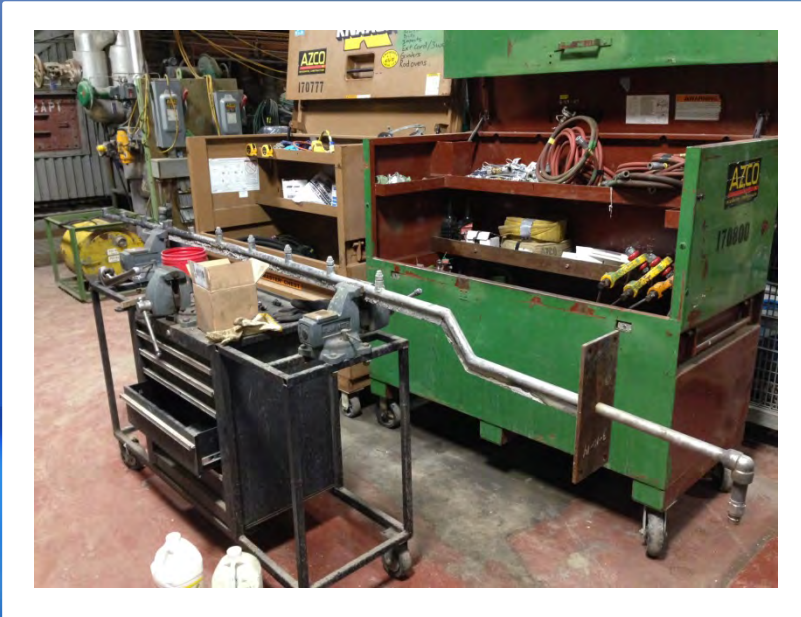


Contours of Mass fraction of h2o

CFD Analysis (4 Nozzle Configuration)



CFD Analysis (8 Nozzle Configuration)



New Lances

- Supplied with high pressure water only
- Angled for structural rigidity



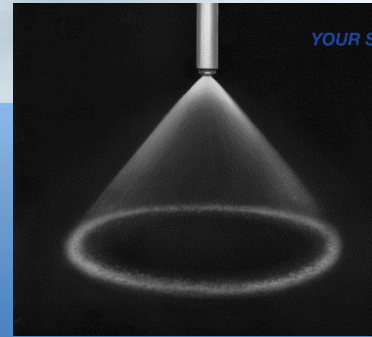
Simplified Pump Skid

Case Study – Equipment Install

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Fabricated from Hastelloy to prevent corrosion
Nozzles have been in operation for 3+ years
Operating at ~ 1,300 psig



We shutdown (2-1/2X) 275 HP rotary screw compressors

- Replaced compressor demands with (3X) 30HP Diaphragm Pumps (VFD)
 - 3 Total (1 per unit) with 1 on standby

Lime consumption ~ 1/2 of 2010 timeframe

SO₂ outlets in single digits

SO₂ & HCL removal in mid to high 90(+)% removal efficiencies

Reduced lance/nozzle cleaning on U1 from weekly to every outage (4 months) – (36X) nozzles without screens

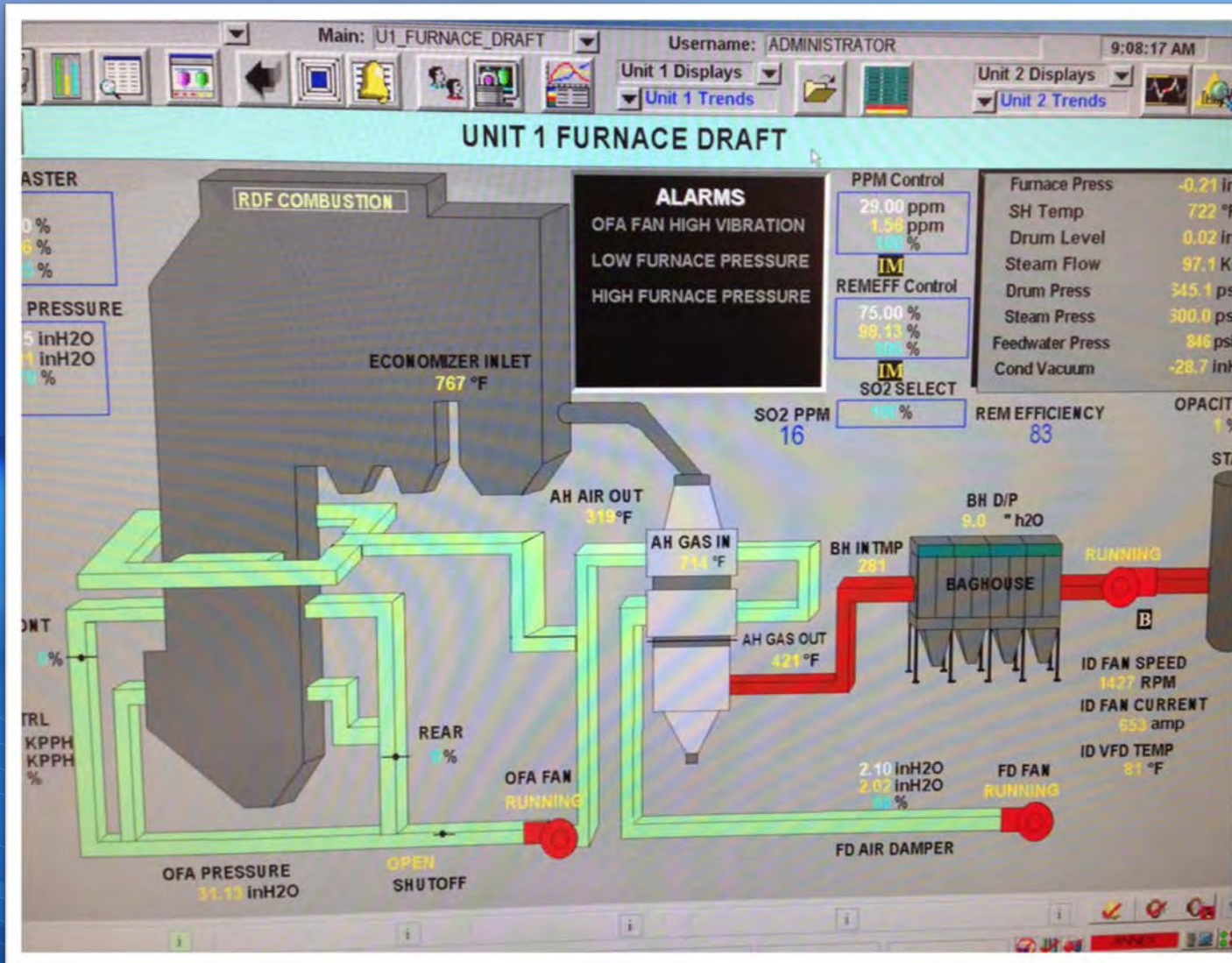
Reduced lance/nozzle cleaning on U2 from weekly to every 2 to 3 weeks – (60X) nozzles with screens

Case Study – Results & Findings – Summary



Category	Original Nozzles	New Nozzles
Nozzle cleaning frequency	Once a week	Once every 2-3 Weeks
Required maintenance	Once a week	General inspection
Nozzle Life	6 months	12-18 months
Compressed air	1,500 SCFM	None
Water Injection Rate	Up to 16 GPM	Up to 25 GPM
Moisture	Wetting of duct	Dry duct
Hopper Plugging Frequency	Frequent	None
Observation by Plant (No firm data)	Unreliable system with high operational costs of compressors	Reliable system with reduced operational and maintenance costs
Annual Maintenance Costs	\$ 25,000+	< \$ 10,000

Case Study - Control Room Data



Case Study – Nozzle Installation

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Upstream Duct Humidification/Cooling before DSI is a viable technology for process improvements

- ✓ Proper Fluid Application Engineering must be performed for successful installation, commissioning, and operation.
- ✓ Each installation is unique.
- ✓ CFD analysis is recommended to ensure proper performance.
- ✓ Downstream effects of lower gas temperature need to be analyzed.
- ✓ Twin-fluid nozzle technology provides the smallest droplet size and highest turndown but may not be most efficient and effective design.



Thank you for your attention!

As an international company Lechler is represented
in more than 50 countries world-wide.

For contact details and more information please visit
our website.

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